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EXPERIMENTAL TEST OF A NEW COMPOSITE MATERIAL

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Abstract: This paper presents extended researches regarding tensile and three-point bend tests accomplished on "SDV" composite material. The experimental tests have been carried out on LS100 Plus and LR5K Plus materials testing machines produced by Lloyd Instruments, UK. Load-extension and load-deflection distributions have been plotted during tensile and three-point bend tests. The tests put into evidence the significant anisotropy of this composite material. **Keywords:** SDV, composite material, tensile test, three-point bend test, load-extension distributions

1. INTRODUCTION

A homogenization method and some averaging methods to predict the elastic properties of multiphase preimpregnated composite materials like Sheet Molding Compounds (SMCs) are presented in reference [1]. The upper and lower limits of the homogenized coefficients for a 27% fibers volume fraction SMC have been computed. A comparison between the upper and lower limits of the homogenized elastic coefficients for a 27% fibers volume fraction SMC and the experimental data is presented. The estimation model used as a homogenization method of these heterogeneous composite materials, gave emphasis to a good agreement between this theoretical approach and experimental data. Hysteresis behaviors of three-phase randomly oriented glass fiber-ceramic particles-reinforced polyester resin composite material subjected to static cyclic tensioncompression loadings have been carried out [2]. Various cyclic tests with different test speeds, load limits and number of cycles have been accomplished on a Lloyd Instruments LS100Plus materials testing machine with STGA/50/50 E85454 extensioneter. The most important results regarding mechanical properties of three-phase chopped strand mat-Al₂O₃ particles-SYNOLITE 8388 P2 polyester resin laminates subjected to short time static cyclic tension-compression loadings are presented in reference [3]. Simulations regarding the elastic properties of glass, carbon and Kevlar49 fiber-reinforced composite laminates based on epoxy resin and subjected to offaxis loading system have been accomplished using an approach developed by Clyne and Withers within Cambridge University, UK [4]. Behavior simulations of various polymer matrix composite laminates subjected to three and four-point bending using the finite element method have been carried out. The models have been designed and analyzed with MSC Patran and MSC Nastran. Four types of composite laminates have been developed based especially on epoxy resin reinforced with Chopped Strand Mats of various specific weights and RT800 glass fabrics [5]. Three types of composite laminates have been subjected to four-point bend tests using the resistive stress analysis have been used in reference [6]. Between these layers, three strain gages have been applied and connected to a Spider8 device. Distributions of load versus time as well as specific deformation versus time for all three types of composite laminates have been experimental determined in four-point bend tests using the CATMAN software. Basic mechanical properties have been experimentally determined on twelve layers glass fabric-reinforced polyester resin specimens subjected to tensile loads on weft direction until break. Glass fabric of type RT300 has been used to reinforce Polylite 440-M888 polyester resin [7]. The most important mechanical properties determined in a simple tensile test on a 0.4 mm thickness 2/2 carbon twill weave fabric impregnated with epoxy resin, used as skins for an advanced ultralight sandwich composite structure with expanded polystyrene as core have been presented in reference [8]. To use composites in design of car components, their mechanical properties are for a great importance. A calculation of the stresses and loads of parts manufactured from composites can be carried out. To determine their mechanical properties, theoretical models can be used. Bearing in mind the differences in the charges of composite materials, even when the same manufacturer produces them, an experimental research is required on these materials [9]. Stratimat 300 glass fibers has been used to reinforce Heliopol 9431ATYX LSE resin in hand lay-up process. A 6 mm thick composite laminate plate with five layers has been cured from which nine specimens have been cut using a diamond powder mill being under protection of a specific cooling system. Interesting mechanical properties have been also determined during three-point bend tests [10]. Other important mechanical characteristics of different composite materials have been presented in references [11-17].

2. THE EXPERIMENTAL SET-UP AND PROCEDURE

The tests in the Scientific Research Contract no. 178 / 8.06.2015 /7284/25.06.2015 "MECHANICAL TENSILE AND BENDING TESTS FOR STANDARD COMPOSITE MATERIAL SPECIMEN" were carried out in the Mechanical Testing Laboratory of the Mechanical Engineering Department within the Faculty of Mechanical Engineering of the Transilvania University of Brasov. The tensile test was performed on the Lloyd LS 100 machine (Fig. 1) with a maximum load of 98 kN. An Epsilon extensometer have been used to determine the strain (Fig. 2). The three-point bend tests have been performed on the Lloyd LR5k machine (Fig. 3) with a maximum load of 5 kN. Specimens provided for tensile testing from the SDV die material are shown in Fig. 4. For three-point bend tests, the SDV material samples are shown in Fig. 5. The dimensions of the specimens have been measured.



Figure 1: The LS100 Plus materials testing machine



Figure 3: The LR5K Plus materials testing machine



Figure 2: The Epsilon extensometer



Figure 4: "SDV" composite specimens for tensile tests



Figure 5: "SDV" composite specimens for three-point bend tests

3. RESULTS

For the SDV composite, load-extension distributions of all specimen, obtained in tensile tests are presented in Figs. 6-8. Figs. 9-11 shows the load-deflection distribution of the specimens, determined in three-point bend tests. Geometrical features of SDV composite specimens for tensile and three-point bend tests are shown in Tables 1 and 2. The tensile and three-point bend tests results are presented in Tables 3 and 4.



Figure 6: Load-extension distribution of SDV1 specimen in tensile test



Figure 8: Load-extension distribution of SDV3 specimen in tensile test



Figure 7: Load-deflection distribution of SDV2 specimen in tensile test



Figure 9: Load-deflection distribution of SDV1 specimen in three-point bend test

 Table 1: Geometric features of SDV composite specimens for tensile tests

Specimen	L (mm)	b (mm)	h (mm)	Area (mm ²)	
SDV1	150	10	5	50	
SDV2	150	10	5	50	
SDV3	150	10	5	50	





Figure 10 Load-deflection distribution of SDV2 specimen in three-point bend test

Figure 11: Load-deflection distribution of SDV3 specimen in three-point bend test

Table 2: Geometric fea	eatures of SDV composite	specimens for three-	point bend tests
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Specimen	L (mm)	b (mm)	h (mm)	Span (mm)	Strength modulus (mm ³)
SDV1	80	10	4.5	64	33.75
SDV2	80	10	4.5	64	33.75
SDV3	80	10	4.5	64	33.75

Specimen	SDV1	SDV2	SDV3	Mean	
Maximum load (N)	3704.3	4382.9	4709.5	4265.6	
Maximum stress (MPa)	74.087	87.657	94.190	85.311	
Deformation at max. load (mm)	0.962	1.038	1.08	1.03	
Strain at max. load (%)	1.9246	2.0764	2.1691	2.0567	
Work at max. load (Nmm)	2075	2677	2929	2560	
Young's modulus (MPa)	6111.4	6604.2	5921.2	6212.2	
Stiffness (N/m)	6111390	6604151	5921200	6212200	

 Table 3: SDV composite tensile test results

Table 4: SDV composite three-point bend test result

Specimen	SDV1	SDV2	SDV3	Mean
Maximum load (N)	294.55	277.57	328.14	300.09
Maximum stress (MPa)	139.64	131.59	155.56	142.26
Deflection at max. load (mm)	9.00	8.34	9.17	8.84
Strain at max. load (%)	5.9326	5.4968	6.0449	5.8248
Work at max. load (Nmm)	1516	1398	1778	1564
Young's modulus of bending(MPa)	3340.0	3793.1	3940.7	3691.3
Stiffness (N/m)	46441	52742	54794	51326
Rigidity at bending (Nm ²)	0.25363	0.28804	0.29925	0.28031

3. CONCLUSION

The tensile and three-point bend tests put into evidence the significant anisotropy of this composite material. The most important mechanical properties have been determined in the tensile test. Among these mechanical features, the Young's modulus determined in tensile tests is for a great importance for future modeling and loading simulations of this composite.

REFERENCES

- [1] Teodorescu-Draghicescu, H., Vlase, S., Homogenization and Averaging Methods to Predict Elastic Properties of Pre-Impregnated Composite Materials, Comp. Mater. Sci., 2011, 50, 4, 1310-1314.
- [2] Teodorescu-Draghicescu, H., Vlase, S., Scutaru, L., Serbina, L., Calin, M.R., Hysteresis Effect in a Three-Phase Polymer Matrix Composite Subjected to Static Cyclic Loadings, Optoelectron. Adv. Mat., 2011, 5, 3, 273-277.
- [3] Vlase, S. Teodorescu-Draghicescu, H., Motoc, D.L., Scutaru, M.L., Serbina, L., Călin, M.R., Behavior of Multiphase Fiber-Reinforced Polymers Under Short Time Cyclic Loading, Optoelectron. Adv. Mat., 2011, 5, 4, 419-423.
- [4] Vlase, S. Teodorescu-Draghicescu, H., Călin, M.R., Serbina, L., Simulation of the Elastic Properties of Some Fibre-Reinforced Composite Laminates Under Off-Axis Loading System, Optoelectron. Adv. Mat., 2011, 5, 4, 424-429.
- [5] Teodorescu-Draghicescu, H., Stanciu, A., Vlase, S., Scutaru, L., Călin M.R., Serbina, L., Finite Element Method Analysis Of Some Fibre-Reinforced Composite Laminates, Optoelectron. Adv. Mat., 2011, 5, 7, 782-785.
- [6] Stanciu, A., Teodorescu-Draghicescu, H., Vlase, S., Scutaru, M.L., Călin, M.R., Mechanical Behavior of CSM450 and RT800 Laminates Subjected to Four-Point Bend Tests, Optoelectron. Adv. Mat., 2012, 6, 3-4, 495-497.
- [7] Vlase, S., Teodorescu-Draghicescu, H., Călin, M.R., Scutaru, M.L., Advanced Polylite composite laminate material behavior to tensile stress on weft direction, J. Optoelectron. Adv. M., 2012, 14, 7-8, 658-663.
- [8] Teodorescu-Draghicescu, H., Scutaru, M.L., Rosu, D., Calin, M.R., Grigore, P., New Advanced Sandwich Composite with twill weave carbon and EPS, J. Optoelectron. Adv. M., 2013, 15, 3-4, 199-203.
- [9] Modrea, A., Vlase, S., Teodorescu-Draghicescu, H., Mihalcica, M., Calin, M.R., Astalos, C., Properties of Advanced New Materials Used in Automotive Engineering, Optoelectron. Adv. Mat., 2013, 7, 5-6, 452-455.
- [10] Vlase, S., Purcarea, R., Teodorescu-Draghicescu, H., Calin, M.R., Szava, I., Mihalcica, M., Behavior of a new Heliopol/Stratimat300 composite laminate, Optoelectron. Adv. Mat., 2013, 7, 7-8, 569-572.
- [11] Heitz, T., Teodorescu-Draghicescu, H., Lache, S., Chiru, A., Calin, M.R., Advanced T700/XB3585 UD carbon fibers-reinforced composite, J. Optoelectron. Adv. M., 2014, 16, 5-6, 568-573.
- [12] Teodorescu-Draghicescu, H., Vlase, S., Stanciu, M.D., Curtu, I., Mihalcica, M., Advanced Pultruded Glass Fibers-Reinforced Isophtalic Polyester Resin, Mater. Plast., 2015, 52, 1, 62-64.
- [13] Scutaru, M.L., Teodorescu-Draghicescu, H., Vlase, S., Marin, M., Advanced HDPE with increased stiffness used for water supply networks, J. Optoelectron. Adv. M., 2015, 17, 3-4, 484-488.
- [14] Modrea, A., Gheorghe, V., Sandu, V., Teodorescu-Draghicescu, H., Mihalcica, M., Scutaru, M.L., Study of a New Composite Material Rt800 Reinforced with Polyte 440-M888 in Endurance Conditions, Procedia Technology, 2016, 22, 182-186.
- [15] Teodorescu-Draghicescu, H., Gheorghe, V., Munteanu, R., Szava, I., Modrea, A., Advanced RT300 Glass Fabric/Polylite Composite Laminate Simulation, Procedia Engineering, 2017, 181, 293-299.
- [16] Teodorescu-Draghicescu, H., Scarlatescu, D., Vlase, S., Scutaru, M.L., Nastac, C., Advanced highdensity polyethylene used in pipelines networks, Procedia Manufacturing, 2018, 22, 27-34.
- [17] Stanciu, M.D., Ardeleanu, A.F., Teodorescu-Draghicescu, H., Reverse engineering in finite element analysis of the behaviour of lignocellulosic materials subjected to cyclic stresses, Procedia Manufacturing, 2018, 22, 65-72.